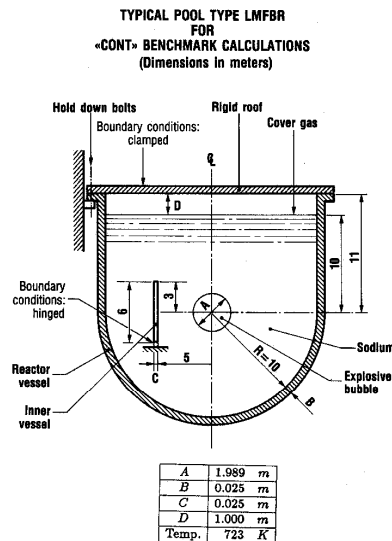


## Exercise/Example 4 – CONT problem

Three fluids plus deformable structures

- Try out ALE solution with Lagrangian fluid/fluid interfaces (single-component fluid model)
- Try out ALE solution with ALE fluid/fluid interfaces (multi-phase multi-component fluid model)



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This is a well-known reactor safety benchmark problem from the 1970's/80s.

### Geometric data:

Simplified sodium-cooled fast breeder reactor (axisymmetric) with internal shield.  
The roof is rigid.

### Materials

The explosive bubble is made of a mixture of molten fuel and fluid sodium (corium).  
The pool is filled by liquid sodium. An argon cover gas fills the region below the roof.  
The tank and inner shield are made of elasto-plastic steel.

### Numerical Solution

### **CONT01**

We use the standard single-component fluid material model. This means that the two fluid-fluid interfaces are treated as Lagrangian. Due to sliding of the sodium/argon interface along the tank, the FSA model may not be used alone to describe fluid-structure interactions (use is made of Lagrangian sliding locally). The input file is:

```
CONT - 01
*-----
ECHO
/CONV win
*-----Problem type
AXIS WONG ALE tagc
*-----Dimensioning
DIME
PT2L 293 PT3L 70 ZONE 3
ED41 33 FLU1 267 pmat 1
BLQ 100
FSA 100
FSSL 100
UNIL 50

LIAT 900
NALE 1 NBLE 232
MTPO 9 MTEL 8
impa 1 psim 7
TERM
opti noecho
*-----Geometry
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2.55400E+00 3.05750E-01 3.76850E+00 7.37220E-01 3.77790E+00
7.14060E-01 4.92700E+00 1.29800E+00 4.93930E+00 1.27620E+00
6.00390E+00 2.00290E+00 6.01890E+00 1.98290E+00 6.98130E+00
2.84020E+00 6.99880E+00 2.82230E+00 7.84310E+00 3.79620E+00
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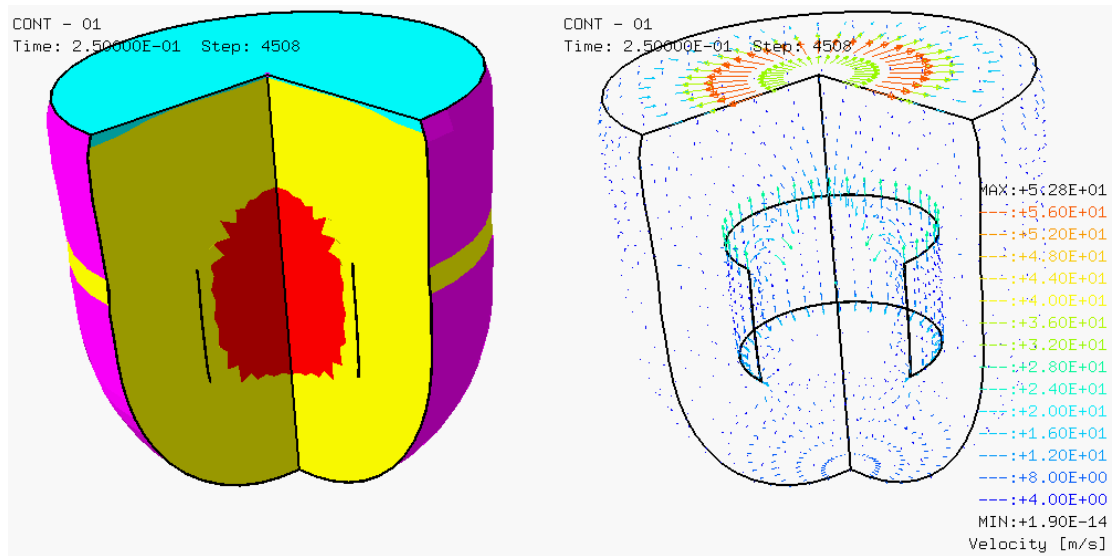
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5.02500E+00 1.18000E+01 5.00000E+01 1.24000E+01 5.02500E+00
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2.54630E+01 9.03310E+00 3.76650E+01 9.07380E+00 4.92430E+01
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9.67800E+02 1.09950E+01 0.00000E+00 1.10000E+01 1.09950E+01
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1.04740E+01 2.09270E+00 1.07040E+01 2.00460E+00 1.09250E+01
1.89300E+01 1.11360E+01 1.76610E+00 1.13250E+00 1.09250E+01
1.14990E+01 1.45770E+00 1.16580E+01 1.27950E+00 1.17990E+01
1.08770E+01 1.19210E+01 8.84300E+01 1.20230E+01 6.71570E+01
1.21030E+01 4.51710E+01 1.21610E+01 2.27060E+01 1.21960E+01
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19
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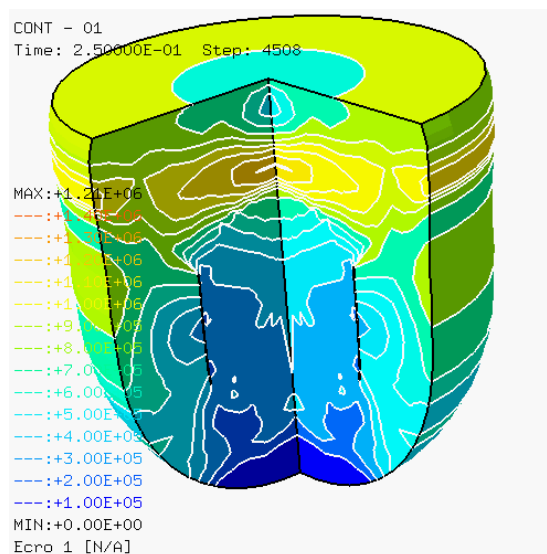
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LECT 6 13 11 325 324 0 0 0 0 1 1 TERM
LECT 7 15 13 326 325 0 0 0 0 1 1 TERM
LECT 8 17 15 327 326 0 0 0 0 1 1 TERM
LECT 9 19 17 328 327 0 0 0 0 1 1 TERM
LECT 10 21 19 329 328 0 0 0 0 1 1 TERM
LECT 11 23 21 330 329 0 0 0 0 1 1 TERM
LECT 12 25 23 331 330 0 0 0 0 1 1 TERM
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LECT 33 69 67 219 217 70 68 220 218 -1 1 TERM
NPOI 28
LAGR NCT1 10
LECT 277 -334 335 TERM
LECT 278 335 336 TERM
LECT 279 336 337 TERM
LECT 280 337 338 TERM
LECT 281 338 339 TERM
LECT 282 339 340 TERM
LECT 283 340 341 TERM
LECT 34 199 221 TERM
LECT 35 221 341 TERM
LECT 292 341 348 TERM
NPOI 11
NCT2 8
LECT 16 -31 33 TERM
LECT 17 33 35 TERM
LECT 18 35 37 TERM
LECT 19 37 39 TERM
LECT 20 39 41 TERM
LECT 21 41 43 TERM
LECT 22 43 45 TERM
LECT 23 45 47 TERM
NPOI 9
*-----Outputs
ECRIURE COOR DEPL VITE CONT ECRO TPRE 250.E-3
POIN LECT 1 74 102 59 69 341 347 43 332 TERM
ELEM LECT 36 63 292 297 34 262 1 21 TERM
fich alic temp FREQ 1
POIN LECT 1 74 102 59 69 341 347 43 332 TERM
ELEM LECT 36 63 292 297 34 262 1 21 TERM
FICH ALIC TPRE 2.5E-3
*-----Options
OPTI AMORT QUAD 2.56 NOTEST
NOCR LECT 292 PAS 1 297 183 196 TERM
cstab 0.45
REZO GAM0 0.8
log 1
*-----Transient calculation
CALC TINI 0.0 DTMI 1E-9 TEND 250.E-3
*-----POST-TREATMENT
SUIT
Post-treatment
ECHO
RESU ALIC TEMP GARD PSCR
SORT GRAP
AXTE 1000.0 'Time [ms]'
*-----Curve definitions
COUR 1 'dy 1' DEPL COMP 2 NOEU LECT 1 TERM
COUR 2 'dy 341' DEPL COMP 2 NOEU LECT 341 TERM
*-----Plots
ttrac 1 2 axes 1.0 'DISPL. [m]' yzcr
*-----Results qualification
QUAL DEPL COMP 2 LECT 1 TERM REFE -6.27942E-2 TOL 1.E-2
DEPL COMP 2 LECT 341 TERM REFE 4.39215E-1 TOL 1.E-2
*-----
FIN

```

The final mesh (colors indicate materials in this case) and fluid velocities are:



The final fluid pressures:

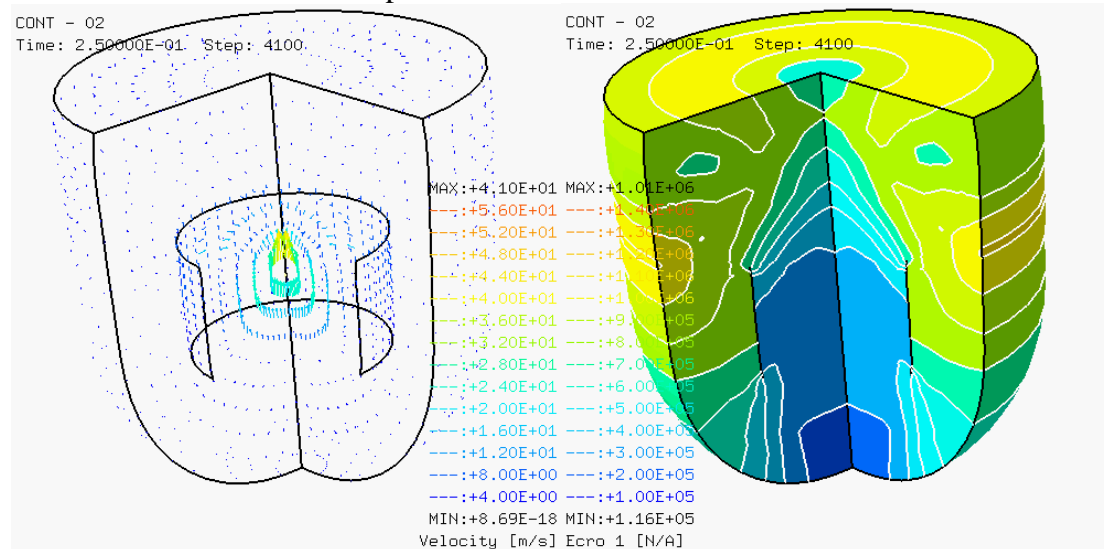


## CONT02

This example uses the multi-phase multi-component fluid material model. This means that the two fluid-fluid interfaces may be treated as ALE and the FSA model may be used to describe fluid-structure interactions. The input file is:

```
CONT - 02
*-----
ECHO
CAST mesh
!CONV win
*-----
AXIS NONL ALE
*-----
DIME
PTL 278 PTL 35 ZONE 3
ED01 33 FL24 230 FL23 28
NALB 18 NBLE 278
MPO 29
MTEL 24
ECRO 13128
TERM
*-----
GEOM ED01 stru FL23 flui3 FL24 flui4 TERM
*-----
COMP EPA1 2.5E-2 LECT stru TERM
*-----
GRIL LAGR LECT stru TERM
ALE LECT flui TERM
AUTO AUTR
*-----
MATE VM23 RO 7800. YOUN 1.6E11 NU 0.333 ELAS 1.05E8
TRAC 2 1.05E8 .65625E-3 1.6105E10 1.00066
LECT vessel TERM
VM23 RO 7800. YOUN 1.6E11 NU 0.333 ELAS 1.05E8
TRAC 2 1.05E8 .65625E-3 1.6105E10 1.00066
LECT shield TERM
FLMP NLIQ 1 NGAS 2
FLUT RO 832. EINT 98.68 GAMM 7.15D0 CL 0.5 CQ 2.56
PB 2.71E5 PMIN 0. AHGF 0. ITER 2 ALFO 1.
BETO 1. KINT 0 NUM 5
LECT liq TERM
FLUT RO 2.4278E3 EINT 0. GAMM 0.75D0 CL 0.5 CQ 2.56
PB 0. PMIN 0. AHGF 0. ITER 2 ALFO 1.
BETO 1. KINT 0 NUM 4
*-----
LECT bull TERM
FLUT RO .242777373 EINT 6.865E5 GAMM 1.6 CL 0.5 CQ 2.56
PB 0. PMIN 0. AHGF 0. ITER 2 ALFO 1.
BETO 1. KINT 0 NUM 1
LECT gas TERM
*-----
LINK COUP
BLOQ 1 LECT p2p TERM
BLOQ 123 LECT p4p TERM
CONT SPLA NX 1 NY 0 LECT symax TERM
CONT SPLA NX 0 NY 1 LECT top TERM
FSA LECT fsan TERM
*-----
ECRI COOR DEPL VITE ACE CONT ECRO TPRE 250.E-3
FICH ALIC TEMP FREQ 1
POIN LECT p0 TERM
FICH ALIC TPRE 2.5E-3
*-----
OPTI NOTE
log 1 csta 0.5
REZO GAMO 0.8
FLMP EPS1 1.E-5
*-----
CALCUL TINI 0.0 TEND 250.E-3
*-----
SUIT
ECHO
RESU ALIC TEMP GARD PSCR
SORT GRAP
AXTE 1000.0 'Time [ms]'
*-----
COUR 1 'dy 1' DEPL COMP 2 NOEU LECT p0 TERM
*-----
TITAC 3 axes 1.0 'DISPL. [m]' yzer
*-----
QUAL DEPL COMP 2 LECT p0 TERM REFE -1.23718E-1 TOL 1.E-2
*-----
FIN
```

The final fluid velocities and pressures:



The final bubble material mass fraction (giving an idea of the size and form of the bubble) and an intermediate time view of the liquid sodium mass fraction:

